Image amplitudes in reverse time migration/inversion

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RTM based linearized inversion

- Seismic imaging is mathematically treated as a linearized inverse problem
- Kirchhoff migration can correspond to a method for inverting discontinuities (Beylkin, 1985).
- There are conditions on the background medium. Single source: no multipathing. Multisource: Traveltime Injectivity Condition (Rakesh, 1988; Nolan and Symes 1997; Ten Kroode Et Al., 1998)
- RTM has the advantage that there are no approximations from ray-theory and one-way methods. We will do linearized inverse scattering by a modified reverse time migration (RTM algorithm

The linearized inverse problem

Source field $u_{\rm src}$

$$\left(rac{1}{{f v}^2}\partial_t^2-
abla_{f x}^2
ight)u_{
m src}({f x},t)=\delta({f x}-{f x}_{
m src})\delta(t)$$

Scattered field: Linearize in the velocity $\frac{1}{v(\mathbf{x})^2} \rightarrow \frac{1}{v(\mathbf{x})^2}(1 + r(\mathbf{x}))$. v the smooth velocity model, r contains singularities

$$\left(rac{1}{v^2}\partial_t^2 -
abla_{\mathbf{x}}^2
ight)u_{
m scat}(\mathbf{x},t) = -rac{r}{v^2}\partial_t^2 u_{
m src}.$$

Problem: Determine $r(\mathbf{x})$ from the following data:

 $u_{ ext{scat}}(\mathbf{x},t)$ for $\mathbf{x}=(x_1,x_2,x_3)$ in a subset of $x_3=0$, $t\in[0,T_{ ext{max}}]$

A new view on Reverse Time Migration

- Numerically solve wave equation to obtain u_{src}(x, t) = incoming (source) wave field u_{rtc}(x, t) = reverse time continued receiver field
- New imaging condition

$$I(\mathbf{x}) = \frac{2i}{2\pi\omega^3} \int \frac{\omega^2 \,\widehat{u}_{\rm src}(\mathbf{x},\omega) \widehat{u}_{\rm rtc}(\mathbf{x},\omega) - v^2 \,\overline{\nabla} \widehat{u}_{\rm src}(\mathbf{x},\omega) \overline{\nabla} \widehat{u}_{\rm rtc}(\mathbf{x},\omega)}{|\widehat{u}_{\rm src}(\mathbf{x},\omega)|^2} \, d\omega.$$

(cf. Kiyashchenko et al., 2007)

Characterization of I

$$I(\mathbf{x}) = R(\mathbf{x}, D_{\mathbf{x}})r,$$

Here R is a pseudodifferential operator that describes the aperture effect, i.e. $R(\mathbf{x}, \boldsymbol{\xi}) = 1$ for "visible" reflectors (cf. Beylkin, 1985).

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Model problem

Notation $\mathbf{x} = (x_1, x_2, x_3)$.

Source field is plane wave with velocity (0, 0, v)

$$u_{\rm src}(\mathbf{x},t) = A \,\delta(t-\frac{x_3}{v})$$

Scattered field slightly simplified

$$\left(\frac{1}{v^2}\partial_t^2 - \nabla_{\mathbf{x}}^2\right)u_{\mathrm{scat}}(t,\mathbf{x}) = A\,\delta(t-\frac{x_3}{v})r(\mathbf{x}).$$

Perfect backpropagation: u_{rtc} solution of a final value problem

$$(rac{1}{v^2}\partial_t^2 -
abla_{\mathbf{x}}^2)u_{
m rtc}(\mathbf{x}, t) = 0$$

 $u_{
m rtc}(\mathbf{x}, T_1) = u_{
m scat}(\mathbf{x}, T_1), \qquad \partial_t u_{
m rtc}(\mathbf{x}, T_1) = \partial_t u_{
m scat}(\mathbf{x}, T_1), \qquad x \in \mathbb{R}^3.$

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Solving the wave equation

Spatial Fourier transform

$$(\mathbf{v}^{-2}\partial_t^2 + \boldsymbol{\xi}^2)\,\widehat{u}(\boldsymbol{\xi},t) = \widehat{f}(\boldsymbol{\xi},t).$$

Duhamel's principle: Let $\widehat{w}(\boldsymbol{\xi}, t, s)$

$$egin{aligned} &(v^{-2}\partial_t^2+m{\xi}^2)\widehat{w}(m{\xi},t,s,)=0,\ &\widehat{w}(m{\xi},s,s)=0 & \partial_t\widehat{w}(m{\xi},s,s)=v^2\widehat{f}(s,\xi). \end{aligned}$$

Result

$$\widehat{u}(\boldsymbol{\xi},t) = \int_0^t \left(e^{iv \|\boldsymbol{\xi}\|(t-s)} - e^{-iv \|\boldsymbol{\xi}\|(t-s)} \right) \frac{v^2 \,\widehat{f}(\boldsymbol{\xi},s)}{2iv \|\boldsymbol{\xi}\|} \, ds$$

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Needed: Fourier transform of r.h.s. $A \delta(t - \frac{x_3}{v}) r(\mathbf{x})$

Fourier transform $f(\mathbf{x}, t) = A \,\delta(t - \frac{x_3}{v}) r(\mathbf{x})$

$$\widehat{f}(\boldsymbol{\xi},t) = \int A\,\delta(t-\frac{x_3}{v})r(\mathbf{x})e^{-i\mathbf{x}\cdot\boldsymbol{\xi}}\,d\mathbf{x}$$
$$= vA\,\mathcal{F}_{(x_1,x_2)\mapsto(\xi_1,\xi_2)}r(\xi_1,\xi_2,v_0t)e^{-i\xi_3vt}.$$

Computations involve two similar terms, take only one of those.

$$\begin{aligned} \widehat{u}_{\text{scat}}(\boldsymbol{\xi},t) &= \int_{0}^{t} \frac{v^{3}}{-2iv \|\boldsymbol{\xi}\|} e^{-iv \|\boldsymbol{\xi}\|(t-s)-i\xi_{3}vs} A \,\mathcal{F}_{(x_{1},x_{2})\mapsto(\xi_{1},\xi_{2})} r(\xi_{1},\xi_{2},vs) \, ds \\ &+ \text{pos. freq. term} \\ &= \frac{Av^{2}}{-2iv \|\boldsymbol{\xi}\|} e^{-iv \|\boldsymbol{\xi}\|t} \, \widehat{r}(\xi_{1},\xi_{2},\xi_{3}-\|\boldsymbol{\xi}\|) + \text{pos. freq. term,} \end{aligned}$$

if t is after the incoming has passed supp(r)Back to space domain

$$u_{\text{scat}}(\mathbf{x},t) = 2 \operatorname{Re} \frac{1}{(2\pi)^3} \int \frac{Av^2}{-2iv \|\boldsymbol{\xi}\|} e^{i\mathbf{x}\cdot\boldsymbol{\xi}-iv \|\boldsymbol{\xi}\|t} \,\widehat{r}(\boldsymbol{\xi}-(0,0,\|\boldsymbol{\xi}\|)) \, d\boldsymbol{\xi}$$

Interpretation

Scattered field

$$u_{\rm scat}(\mathbf{x},t) = 2 \operatorname{Re} \frac{1}{(2\pi)^3} \int \frac{Av^2}{-2iv \|\xi\|} e^{i\mathbf{x}\cdot\boldsymbol{\xi} - iv \|\boldsymbol{\xi}\|t} \, \widehat{r}(\boldsymbol{\xi} - (0,0,\|\boldsymbol{\xi}\|)) \, d\boldsymbol{\xi}$$

Wave vectors

$$\begin{split} & \boldsymbol{\xi} \\ & (0,0,\|\boldsymbol{\xi}\|) \\ & \boldsymbol{\xi} - (0,0,\|\boldsymbol{\xi}\|) \end{split}$$

outgoing wave number incoming wave number reflectivity wave number



Modified excitation time imaging condition

Same formula for the backpropagated field! Valid for all t

$$u_{\rm rtc}(\mathbf{x},t) = 2\operatorname{Re}\frac{1}{(2\pi)^3}\int \frac{Av^2}{-2iv\|\boldsymbol{\xi}\|} e^{i\mathbf{x}\cdot\boldsymbol{\xi}-iv\|\boldsymbol{\xi}\|t} \,\widehat{r}(\boldsymbol{\xi}-(0,0,\|\boldsymbol{\xi}\|)) \,d\boldsymbol{\xi}$$

Basic image: $I_0(\mathbf{x}) = u_{\text{rtc}}(\mathbf{x}, x_3/v)$.

Linearized inverse scattering: Try

$$I(\mathbf{x}) = \frac{2}{v^2 A} \left(\partial_t + v \partial_{x_3} \right) u_{\rm rtc}(\mathbf{x}, x_3/v)$$

(meaning first take derivatives then insert $(\mathbf{x}, t) = (\mathbf{x}, x_3/v)$) Straightforward calculation yields

$$I(\mathbf{x}) = 2 \operatorname{Re} \frac{1}{(2\pi)^3} \int_{\mathbb{R}^3} \left(1 - \frac{\xi_3}{\|\boldsymbol{\xi}\|} \right) \widehat{r}(\boldsymbol{\xi} - (0, 0, \|\boldsymbol{\xi}\|)) d\boldsymbol{\xi}$$

A change of variables

Copy from previous slide:

$$I(\mathbf{x}) = 2 \operatorname{Re} \frac{1}{(2\pi)^3} \int_{\mathbb{R}^3} \left(1 - \frac{\xi_3}{\|\boldsymbol{\xi}\|} \right) \widehat{r}(\boldsymbol{\xi} - (0, 0, \|\boldsymbol{\xi}\|)) d\boldsymbol{\xi}$$



Result:

$$I(\mathbf{x}) = 2 \operatorname{Re} \frac{1}{(2\pi)^3} \int_{\mathbb{R}^2 \times \mathbb{R}_{<0}} \widehat{r}(\tilde{\boldsymbol{\xi}}) e^{i\mathbf{x}\cdot\tilde{\boldsymbol{\xi}}} d\tilde{\boldsymbol{\xi}} = \frac{1}{(2\pi)^3} \int_{\mathbb{R}^2 \times \mathbb{R}_{\neq 0}} \widehat{r}(\tilde{\boldsymbol{\xi}}) e^{i\mathbf{x}\cdot\tilde{\boldsymbol{\xi}}} d\tilde{\boldsymbol{\xi}}.$$

Reconstruction except for $\xi_3 = 0$, corresponding to reflection over 180 degrees.

Modified ratio imaging condition

We had

$$I(\mathbf{x}) = \frac{2}{v^2 A} \left(\partial_t + (0, 0, v) \cdot \nabla_{\mathbf{x}} \right) u_{\text{rtc}}(\mathbf{x}, x_3/v)$$

Rewrite into modified ratio imaging condition

• Use that $(0,0,v) = v^2 \nabla T(\mathbf{x})$, and that

$$\widehat{u}_{\rm src}(\mathbf{x},\omega) = Ae^{-i\omega T(\mathbf{x})},$$
$$\nabla_{\mathbf{x}} \widehat{u}_{\rm src}(\mathbf{x},\omega) \approx -i\omega \nabla_{\mathbf{x}} T(\mathbf{x}) Ae^{-i\omega T(\mathbf{x})}$$

▶ Insert factors $\frac{v^2}{\omega^2}$ left out in model problem This results in

$$I(\mathbf{x}) = \frac{2i}{2\pi\omega^3} \int \frac{\omega^2 \,\overline{\widehat{u}_{\rm src}}(\mathbf{x},\omega) \widehat{u}_{\rm rtc}(\mathbf{x},\omega) - v^2 \,\overline{\nabla \widehat{u}_{\rm src}}(\mathbf{x},\omega) \nabla \widehat{u}_{\rm rtc}(\mathbf{x},\omega)}{|\widehat{u}_{\rm src}(\mathbf{x},\omega)|^2} \, d\omega.$$

Extension to variable background

Local vs. global analysis

- A local analysis generalizes the explicit formulas to variable coefficients, and leads to explicit inversion formulas
- A global analysis takes into account the of global effect of curved rays. No source-multipathing is allowed to exclude kinematic artifacts ("cross talk"). Cf. Rakesh (1988), Nolan and Symes (1997).

Tools: microlocal analysis

- Fourier integral operators (FIO's), pseudodifferential operators (VDO's)
- Description of the mapping properties of operators for localized plane wave components. Work in (x, ξ) or (x, t, ξ, ω) domain.

Variable coefficients: The wave equation

Local analysis

Solve the wave equation using WKB with plane wave initial values. Result is an $\ensuremath{\mathsf{FIO}}$

$$u(\mathbf{y},t) = \frac{1}{(2\pi)^3} \iint e^{i\alpha(\mathbf{y},t-s,\boldsymbol{\xi})} a(\mathbf{y},t-s,\boldsymbol{\xi}) \widehat{f}(\boldsymbol{\xi},s) \, ds \, d\boldsymbol{\xi} + \text{pos. freq. term},$$

 α satisfies the eikonal equation; a a transport equation. Formula is valid for t,s in a bounded time interval

Global analysis

- Propagation of localized plane wave components along rays, properly described as curves in (x, t, ξ, ω) space
- Time reversal property is globally valid

Continued scattered field and linearized forward map

Define the continued scattered field u_h , as the "perfect" backpropagated field from a fixed time, full position space

Local result

For a localized contribution to r

$$u_{\mathrm{h,a}}(\mathbf{y},t) = \frac{1}{(2\pi)^3} \iint e^{i\varphi_T(\mathbf{y},t,\mathbf{x},\xi)} A(\mathbf{y},t,\mathbf{x},\xi) \, r(\mathbf{x}) \, d\xi \, d\mathbf{x}.$$

With phase function

$$\varphi_{\mathcal{T}}(\mathbf{y}, t, \mathbf{x}, \xi) = \alpha(\mathbf{y}, t - \mathcal{T}(\mathbf{x}), \xi) - \boldsymbol{\xi} \cdot \mathbf{x}$$

Global result

The map $F_-: r \mapsto u_h$ is a FIO. Mapping of wave components $(\mathbf{x}, \boldsymbol{\zeta}) \mapsto (\mathbf{y}, t, \boldsymbol{\eta}, \omega)$: see picture



RT continuation from the boundary

Preprocess data:

- Ψ DO cutoff $\Psi_M(y_1, y_2, t, \eta_1, \eta_2, \omega)$ with three effects
 - Smooth taper near acquisition boundary
 - Remove direct waves
 - Remove tangently incoming waves

Normalize wave field to get true amplitude time reversal
 Characterize mathematically the aperture effect

Result There are Ψ DO's P_- , P_+ , such that

$$u_{\rm rtc}({\bf x},t) = P_{-}(t,x,D_x)u_{{
m h},-} + P_{+}(t,x,D_x)u_{{
m h},+}$$

in which $u_{\mathrm{h},\pm}$ is the part of u_{h} with $\pm\omega>$ 0. To highest order

$$P_{\pm}(s, \mathbf{x}, \boldsymbol{\xi}) = \Psi_{M}(y_{1}, y_{2}, t, \eta_{1}, \eta_{2}, \omega) \text{ if there is a}$$
ray with $\pm \omega > 0$, connecting $(\mathbf{x}, s, \boldsymbol{\xi}, \omega)$
with $(y_{1}, y_{2}, t, \eta_{1}, \eta_{2}, \omega)$

Inverse scattering

Modified excitation time imaging condition

$$I(\mathbf{x}) = \frac{2}{A_{\rm src}(\mathbf{x})} \partial_t^{-\frac{n+1}{2}} \left[\partial_t + v^2 \nabla T \cdot \nabla_{\mathbf{x}} \right] u_{\rm rtc}(\mathbf{x}, t)$$

 From the global analysis, there are no nonlocal contributions and

$$I(\mathbf{x}) = \Psi DO r(\mathbf{x})$$

From the local analysis

$$I(\mathbf{x}) = (R_{-}(\mathbf{x}, D_{\mathbf{x}}) + R_{+}(\mathbf{x}, D_{\mathbf{x}})) r(\mathbf{x})$$

To highest order

$$R_{\pm}(\mathbf{x},\boldsymbol{\zeta}) = P_{\pm}(\mathbf{x},\boldsymbol{\xi})$$

if $\boldsymbol{\zeta}$ and $\boldsymbol{\xi}$ are related through
$$\boldsymbol{\zeta} = \boldsymbol{\xi} \pm \omega \nabla T(\mathbf{x}).$$

Modified ratio imaging condition derived similarly as above.

Example: A vertical gradient medium



Example 1: Velocity perturbation, reconstructed velocity perturbation, and three traces for background medium v = 2.0 + 0.001z (z in meters and v in km/s). Error 8-10 %.

Example: Horizontal reflector with receiver side caustics



Example 2: (a) A velocity model with some rays; (b) Simulated data, with direct arrival removed; (c) Velocity perturbation; (d) Reconstructed velocity perturbation. Error 0-10%

Conclusion and discussion

- We modified reverse time migration to become a linearized inverse scattering method
- We characterized the resolution operator as a partial inverse, a ΨDO with symbol describing aperture effects
- The modified imaging condition suppresses low-frequency artifacts
- Good numerical results in (bandlimited) examples
- Straightforward generalization of the imaging condition to downward propagation methods

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